## 600kHz/1.2MHz PWM Step-Up Regulator

The EL7516 is a high frequency, high efficiency step-up voltage regulator operated at constant frequency PWM mode. With an internal $1.5 \mathrm{~A}, 200 \mathrm{~m} \Omega$ MOSFET, it can deliver up to 600 mA output current at over $90 \%$ efficiency. The selectable 600 kHz and 1.2 MHz allows smaller inductors and faster transient response. An external compensation pin gives the user greater flexibility in setting frequency compensation allowing the use of low ESR Ceramic output capacitors.

When shut down, it draws $<10 \mu \mathrm{~A}$ of current and can operate down to 2.5 V input supply. These features along with 1.2 MHz switching frequency makes it an ideal device for portable equipment and TFT-LCD displays.

The EL7516 is available in an 8-pin MSOP package with a maximum height of 1.1 mm . The device is specified for operation over the full $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ temperature range.

## Pinout

EL7516
(8-PIN MSOP)
TOP VIEW


## Features

- > 90\% efficiency
- 1.6A, 200m $\Omega$ power MOSFET
- $\mathrm{V}_{\mathrm{IN}}>2.5 \mathrm{~V}$
- $600 \mathrm{kHz} / 1.2 \mathrm{MHz}$ switching frequency selection
- Adjustable soft-start
- Internal thermal protection
- 1.1 mm max height 8-pin MSOP package
- Pb-free available (RoHS compliant)


## Applications

- TFT-LCD displays
- DSL modems
- PCMCIA cards
- Digital cameras
- GSM/CDMA phones
- Portable equipment
- Handheld devices


## Ordering Information

| PART NUMBER | PACKAGE |  <br> REEL | PKG. DWG. \# |
| :--- | :---: | :---: | :---: |
| EL7516IY | 8-Pin MSOP | - | MDP0043 |
| EL7516IY-T7 | 8-Pin MSOP | $7 "$ | MDP0043 |
| EL7516IY-T13 | 8-Pin MSOP | $13^{\prime \prime}$ | MDP0043 |
| EL7516IYZ <br> (See Note) | 8-Pin MSOP <br> (Pb-Free) | - | MDP0043 |
| EL7516IYZ-T7 <br> (See Note) | 8-Pin MSOP <br> (Pb-Free) | $7 "$ | MDP0043 |
| EL7516IYZ-T13 <br> (See Note) | 8-Pin MSOP <br> (Pb-Free) | $13^{\prime \prime}$ | MDP0043 |

NOTE: Intersil Pb -free products employ special Pb -free material sets; molding compounds/die attach materials and $100 \%$ matte tin plate termination finish, which are RoHS compliant and compatible with both SnPb and Pb -free soldering operations. Intersil Pb -free products are MSL classified at Pb -free peak reflow temperatures that meet or exceed the Pb-free requirements of IPC/JEDEC J STD-020C.

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Absolute Maximum Ratings \(\left(\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}\right)\)
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LX to GND . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 18 V
$V_{D D}$ to GND. ...................................................... . . . 6 V
COMP, FB, $\overline{\text { SHDN }}, \mathrm{SS}$, FSEL to GND $\ldots . . .-0.3 \mathrm{~V}$ to $\left(\mathrm{V}_{\mathrm{DD}}+0.3 \mathrm{~V}\right)$

Storage Temperature . . . . . . . . . . . . . . . . . . . . . . . . $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
Operating Ambient Temperature . . . . . . . . . . . . . . . . $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Operating Junction Temperature . . . . . . . . . . . . . . . . . . . . . . +135 ${ }^{\circ} \mathrm{C}$

CAUTION: Stresses above those listed in "Absolute Maximum Ratings" may cause permanent damage to the device. This is a stress only rating and operation of the device at these or any other conditions above those indicated in the operational sections of this specification is not implied.

IMPORTANT NOTE: All parameters having Min/Max specifications are guaranteed. Typical values are for information purposes only. Unless otherwise noted, all tests are at the specified temperature and are pulsed tests, therefore: $T_{J}=T_{C}=T_{A}$

Electrical Specifications $\quad \mathrm{V}_{\mathrm{IN}}=3.3 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=12 \mathrm{~V}$, IOUT $=0 \mathrm{~mA}, \mathrm{FSEL}=\mathrm{GND}, \mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ unless otherwise specified.

| PARAMETER | DESCRIPTION | CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| IQ1 | Quiescent Current - Shut-down | $\overline{\text { SHDN }}=0 \mathrm{~V}$ |  | 0.6 | 10 | $\mu \mathrm{A}$ |
| IQ2 | Quiescent Current - Not Switching | $\overline{\mathrm{SHDN}}=\mathrm{V}_{\mathrm{DD}}, \mathrm{FB}=1.3 \mathrm{~V}$ |  | 0.7 |  | mA |
| IQ3 | Quiescent Current - Switching | $\overline{\mathrm{SHDN}}=\mathrm{V}_{\mathrm{DD}}, \mathrm{FB}=1.0 \mathrm{~V}$ |  | 1.3 | 2 | mA |
| $\mathrm{V}_{\mathrm{FB}}$ | Feedback Voltage |  | 1.272 | 1.294 | 1.309 | V |
| $\mathrm{I}_{\mathrm{B}-\mathrm{FB}}$ | Feedback Input Bias Current |  |  | 0.01 | 0.5 | $\mu \mathrm{A}$ |
| $V_{\text {DD }}$ | Start-Up Input Voltage Range |  | 2.6 |  | 5.5 | V |
| D MAX 600 kHz | Maximum Duty Cycle | FSEL $=0 \mathrm{~V}$ | 84 | 90 |  | \% |
| $\mathrm{D}_{\text {MAX }}-1.2 \mathrm{MHz}$ | Maximum Duty Cycle | FSEL $=\mathrm{V}_{\mathrm{DD}}$ | 84 | 90 |  | \% |
| ILIM | Current Limit - Max Peak Input Current |  | 1.3 | 1.5 |  | A |
| ISHDN | Shut-down Input Bias Current | $\overline{\mathrm{SHDN}}=0 \mathrm{~V}$ |  | 0.01 | 0.1 | $\mu \mathrm{A}$ |
| R ${ }_{\text {DS-ON }}$ | Switch ON Resistance | $\mathrm{V}_{\mathrm{DD}}=2.7 \mathrm{~V}, \mathrm{I}_{\mathrm{LX}}=1 \mathrm{~A}$ |  | 0.2 |  | $\Omega$ |
| lıX-LEAK | Switch Leakage Current | $\mathrm{VSW}=18 \mathrm{~V}$ |  | 0.01 | 3 | $\mu \mathrm{A}$ |
| $\Delta \mathrm{V}_{\text {OUT }} / \Delta \mathrm{V}_{\text {IN }}$ | Line Regulation | $3 \mathrm{~V}<\mathrm{V}_{\text {IN }}<5.5 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=12 \mathrm{~V}$ |  | 0.1 |  | \% |
| $\Delta \mathrm{V}_{\text {OUT }} / \Delta \mathrm{I}_{\text {OUT }}$ | Load Regulation | $\mathrm{V}_{\text {IN }}=3.3 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=12 \mathrm{~V}, \mathrm{I}_{\mathrm{O}}=30 \mathrm{~mA}$ to 200 mA |  | 6.7 |  | mV/A |
| Fosc1 | Switching Frequency Accuracy | FSEL = OV | 500 | 620 | 740 | kHz |
| Fosc2 | Switching Frequency Accuracy | FSEL $=\mathrm{V}_{\mathrm{DD}}$ | 1000 | 1250 | 1500 | kHz |
| $\mathrm{V}_{\text {IL }}$ | SHDN, FSEL Input Low Level |  |  |  | 0.5 | V |
| $\mathrm{V}_{\mathrm{IH}}$ | $\overline{\text { SHDN, }}$, FSEL Input High Level |  | 2.7 |  |  | V |
| $\mathrm{G}_{\mathrm{M}}$ | Error Amp Tranconductance | $\Delta \mathrm{l}=5 \mu \mathrm{~A}$ | 90 | 130 | 170 | $1 \mu / \Omega$ |
| $A_{V}$ | Voltage Gain |  |  | 350 |  | V/V |
| $\mathrm{V}_{\text {DD-ON }}$ | $V_{\text {DD }}$ UVLO On Threshold |  | 2.40 | 2.51 | 2.60 | V |
| $\mathrm{V}_{\text {DD-OFF }}$ | $V_{\text {DD }}$ UVLO Off Threshold |  | 2.20 | 2.30 | 2.40 | V |
| Iss | Soft-start Charge Current |  | 4 | 6 | 8 | $\mu \mathrm{A}$ |
| R CS | Current Sense Transresistance |  |  | 0.08 |  | V/A |
| OTP | Over Temperature Protection |  |  | 130 |  | ${ }^{\circ} \mathrm{C}$ |

## Block Diagram



## Pin Descriptions

| PIN NUMBER | PIN NAME | DESCRIPTION |
| :---: | :---: | :---: |
| 1 | COMP | Compensation pin. Output of the internal error amplifier. Capacitor and resistor from COMP pin to ground. |
| 2 | FB | Voltage feedback pin. Internal reference is 1.294 V nominal. Connect a resistor divider from $\mathrm{V}_{\text {OUT }} . \mathrm{V}_{\text {OUT }}=$ $1.294 \mathrm{~V}\left(1+\mathrm{R}_{1} / \mathrm{R}_{2}\right)$. See Typical Application Circuit. |
| 3 | $\overline{\text { SHDN }}$ | Shutdown control pin. Pull $\overline{\text { SHDN }}$ low to turn off the device. |
| 4 | GND | Analog and power ground. |
| 5 | LX | Power switch pin. Connected to the drain of the internal power MOSFET. |
| 6 | VDD | Analog power supply input pin. |
| 7 | FSEL | Frequency select pin. When FSEL is set low, switching frequency is set to 620 kHz . When connected to high or $\mathrm{V}_{\mathrm{DD}}$, switching frequency is set to 1.25 MHz . |
| 8 | SS | Soft-start control pin. Connect a capacitor to control the converter start-up. |

## Typical Application Circuit



## Typical Performance Curves



FIGURE 1. EFFICIENCY - 3.3V VIN TO $12 \mathrm{~V} \mathrm{~V}_{\text {OUT }} @ 1.3 \mathrm{MHz}$


FIGURE 3. EFFICIENCY - $3.3 \mathrm{~V} \mathrm{~V}_{\mathrm{IN}}$ TO $12 \mathrm{~V} \mathrm{~V}_{\text {OUT }} @ 620 \mathrm{kHz}$


FIGURE 5. EFFICIENCY - $3.3 \mathrm{~V} \mathrm{~V}_{\text {IN }}$ TO $9 \mathrm{~V} \mathrm{~V}_{\text {OUT }}$ @ 1.2 MHz


FIGURE 2. LOAD REGULATION - 3.3V VIN TO $12 \mathrm{~V} \mathrm{~V}_{\mathrm{OUT}}$ @ 1.3MHz


FIGURE 4. LOAD REGULATION - $3.3 \mathrm{~V} \mathrm{~V}_{\mathrm{IN}}$ TO $12 \mathrm{~V} \mathrm{~V}_{\text {OUT }}$ @ 620kHz


FIGURE 6. LOAD REGULATION - 3.3V VIN TO 9V VOUT @ 1.2MHz

## Typical Performance Curves (Continued)



FIGURE 7. EFFICIENCY - $3.3 \mathrm{~V} \mathrm{~V}_{\mathrm{IN}}$ TO $9 \mathrm{~V} \mathrm{~V}_{\mathrm{OUT}} @ 600 \mathrm{kHz}$


FIGURE 9. EFFICIENCY - $5 \mathrm{~V} \mathrm{~V}_{\mathrm{IN}}$ TO $12 \mathrm{~V} \mathrm{~V}_{\text {OUT }} @ 1.2 \mathrm{MHz}$


FIGURE 11. EFFICIENCY-5V VIN TO 12V VOUT @ 600kHz


FIGURE 8. LOAD REGULATION -3.3V $\mathrm{V}_{\text {IN }}$ TO $9 \mathrm{~V} \mathrm{~V}_{\text {OUT }}$ @ 600kHz


FIGURE 10. LOAD REGULATION - $5 \mathrm{~V} \mathrm{~V}_{\mathrm{IN}}$ TO $12 \mathrm{~V} \mathrm{~V}_{\text {OUT }}$ @ 1.2MHz


FIGURE 12. LOAD REGULATION - $5 \mathrm{~V} \mathrm{~V}_{\mathrm{IN}}$ TO 12 V VOUT @ 600kHz

## Typical Performance Curves (Continued)



FIGURE 13. EFFICIENCY - 5V VIN TO 9V VOUT @ 1.2 MHz


FIGURE 15. LINE REGULATION


FIGURE 17. EFFICIENCY vs IOUT - 3.3 V TO 8V


FIGURE 14. LOAD REGULATION - 5V VIN TO 9V VOUT @ 1.2MHz


FIGURE 16. LINE REGULATION


FIGURE 18. LOAD REGULATION - 3.3V TO 8V

## Typical Performance Curves (Continued)



FIGURE 19. EFFICIENCY vs IOUT


FIGURE 21. FREQUENCY ( 600 kHz ) vs $\mathrm{V}_{\text {IN }}$


FIGURE 23. LOAD REGULATION - $5 \mathrm{~V} \mathrm{~V}_{\text {IN }}$ TO $9 \mathrm{~V} \mathrm{~V}_{\text {OUT }}$ @ 600kHz


FIGURE 20. FREQUENCY (1.2MHz) vs $\mathrm{V}_{\text {IN }}$


FIGURE 22. EFFICIENCY-5V $\mathrm{V}_{\text {IN }}$ TO $9 \mathrm{~V} \mathrm{~V}_{\text {OUT }} @ 600 \mathrm{kHz}$


FIGURE 24. TRANSIENT REPONSE - 600kHz

## Typical Performance Curves (Continued)



FIGURE 25. TRANSIENT RESPONSE - 1.2MHz


FIGURE 26. PACKAGE POWER DISSIPATION vs AMBIENT TEMPERATURE


FIGURE 27. PACKAGE POWER DISSIPATION vs AMBIENT TEMPERATURE

## Applications Information

The EL7516 is a high frequency, high efficiency boost regulator operated at constant frequency PWM mode. The boost converter stores energy from an input voltage source and deliver it to a higher output voltage. The input voltage range is 2.5 V to 5.5 V and output voltage range is 5 V to 18 V . The switching frequency is selectable between 600 KHz and 1.2 MHz allowing smaller inductors and faster transient response. An external compensation pin gives the user greater flexibility in setting output transient response and tighter load regulation. The converter soft-start characteristic can also be controlled by external $\mathrm{C}_{\text {SS }}$ capacitor. The $\overline{\text { SHDN }}$ pin allows the user to completely shut-down the device.

## Boost Converter Operations

Figure 28 shows a boost converter with all the key components. In steady state operating and continuous conduction mode where the inductor current is continuous,
the boost converter operates in two cycles. During the first cycle, as shown in Figure 29, the internal power FET turns on and the Schottky diode is reverse biased and cuts off the current flow to the output. The output current is supplied from the output capacitor. The voltage across the inductor is $\mathrm{V}_{\text {IN }}$ and the inductor current ramps up in a rate of $\mathrm{V}_{\text {IN }} / \mathrm{L}, \mathrm{L}$ is the inductance. The inductance is magnetized and energy is stored in the inductor. The change in inductor current is:
$\Delta \mathrm{I}_{\mathrm{L} 1}=\Delta \mathrm{T} 1 \times \frac{\mathrm{V}_{\mathrm{IN}}}{\mathrm{L}}$
$\Delta \mathrm{T} 1=\frac{\mathrm{D}}{\mathrm{F}_{\mathrm{SW}}}$
D = Duty Cycle
$\Delta \mathrm{V}_{\mathrm{O}}=\frac{\mathrm{I}_{\mathrm{OUT}}}{\mathrm{C}_{\text {OUT }}} \times \Delta \mathrm{T}_{1}$

During the second cycle, the power FET turns off and the Schottky diode is forward biased, Figure 30. The energy stored in the inductor is pumped to the output supplying output current and charging the output capacitor. The Schottky diode side of the inductor is clamp to a Schottky diode above the output voltage. So the voltage drop across the inductor is $\mathrm{V}_{\text {IN }}-\mathrm{V}_{\text {OUT }}$. The change in inductor current during the second cycle is:
$\Delta \mathrm{I}_{\mathrm{L}}=\Delta \mathrm{T} 2 \times \frac{\mathrm{V}_{\mathrm{IN}}-\mathrm{V}_{\mathrm{OUT}}}{\mathrm{L}}$
$\Delta T 2=\frac{1-\mathrm{D}}{\mathrm{F}_{\mathrm{SW}}}$
For stable operation, the same amount of energy stored in the inductor must be taken out. The change in inductor current during the two cycles must be the same.
$\Delta I 1+\Delta l 2=0$
$\frac{D}{F_{S W}} \times \frac{V_{I N}}{L}+\frac{1-D}{F_{S W}} \times \frac{V_{I N}-V_{\text {OUT }}}{L}=0$
$\frac{\mathrm{V}_{\text {OUT }}}{\mathrm{V}_{\text {IN }}}=\frac{1}{1-\mathrm{D}}$


FIGURE 28. BOOST CONVERTER


FIGURE 29. BOOST CONVERTER - CYCLE 1, POWER SWITCH CLOSED


FIGURE 30. BOOST CONVERTER - CYCLE 2, POWER SWITCH OPEN

## Output Voltage

An external feedback resistor divider is required to divide the output voltage down to the nominal 1.294 V reference voltage. The current drawn by the resistor network should be limited to maintain the overall converter efficiency. The maximum value of the resistor network is limited by the feedback input bias current and the potential for noise being coupled into the feedback pin. A resistor network less than 100 K is recommended. The boost converter output voltage is determined by the relationship:
$\mathrm{V}_{\mathrm{OUT}}=\mathrm{V}_{\mathrm{FB}} \times\left(1+\frac{\mathrm{R}_{1}}{\mathrm{R}_{2}}\right)$

The nominal VFB voltage is 1.294 V .

## Inductor Selection

The inductor selection determines the output ripple voltage, transient response, output current capability, and efficiency. Its selection depends on the input voltage, output voltage, switching frequency, and maximum output current. For most applications, the inductance should be in the range of $2 \mu \mathrm{H}$ to $33 \mu \mathrm{H}$. The inductor maximum DC current specification must be greater than the peak inductor current required by the regulator. The peak inductor current can be calculated:
$\mathrm{I}_{\mathrm{L}(\mathrm{PEAK})}=\frac{\mathrm{I}_{\mathrm{OUT}} \times \mathrm{V}_{\text {OUT }}}{\mathrm{V}_{\text {IN }}}+1 / 2 \times \frac{\mathrm{V}_{\text {IN }} \times\left(\mathrm{V}_{\text {OUT }}-\mathrm{V}_{\text {IN }}\right)}{\mathrm{L} \times \mathrm{V}_{\text {OUT }} \times \mathrm{FREQ}}$

## Output Capacitor

Low ESR capacitors should be used to minimized the output voltage ripple. Multilayer ceramic capacitors (X5R and X7R) are preferred for the output capacitors because of their lower ESR and small packages. Tantalum capacitors with higher ESR can also be used. The output ripple can be calculated as:
$\Delta \mathrm{V}_{\mathrm{O}}=\frac{\mathrm{I}_{\mathrm{OUT}} \times \mathrm{D}}{\mathrm{F}_{\text {SW }} \times \mathrm{C}_{\mathrm{O}}}+\mathrm{I}_{\mathrm{OUT}} \times \mathrm{ESR}$

For noise sensitive application, a $0.1 \mu \mathrm{~F}$ placed in parallel with the larger output capacitor is recommended to reduce the switching noise coupled from the LX switching node.

## Schottky Diode

In selecting the Schottky diode, the reverse break down voltage, forward current and forward voltage drop must be considered for optimum converter performance. The diode must be rated to handle 1.5A, the current limit of the EL7516. The breakdown voltage must exceed the maximum output voltage. Low forward voltage drop, low leakage current, and fast reverse recovery will help the converter to achieve the maximum efficiency.

## Input Capacitor

The value of the input capacitor depends the input and output voltages, the maximum output current, the inductor value and the noise allowed to put back on the input line. For most applications, a minimum $10 \mu \mathrm{~F}$ is required. For applications that run close to the maximum output current limit, input capacitor in the range of $22 \mu \mathrm{~F}$ to $47 \mu \mathrm{~F}$ is recommended.

The EL7516 is powered from the $\mathrm{V}_{\mathrm{IN}}$. To. High frequency $0.1 \mu \mathrm{~F}$ by-pass cap is recommended to be close to the $\mathrm{V}_{\mathrm{IN}}$ pin to reduce supply line noise and ensure stable operation.

## Loop Compensation

The EL7516 incorporates an transconductance amplifier in its feedback path to allow the user some adjustment on the transient response and better regulation. The EL7516 uses current mode control architecture which has a fast current sense loop and a slow voltage feedback loop. The fast current feedback loop does not require any compensation. The slow voltage loop must be compensated for stable operation. The compensation network is a series RC network from COMP pin to ground. The resistor sets the high frequency integrator gain for fast transient response and the capacitor sets the integrator zero to ensure loop stability. For most applications, the compensation resistor in the range of 2 K to 7.5 K and the compensation capacitor in the range of $3 n F$ to $10 n F$.

## Soft-Start

The soft-start is provided by an internal $6 \mu \mathrm{~A}$ current source charges the external $\mathrm{C}_{S S}$, the peak MOSFET current is limited by the voltage on the capacitor. This in turn controls the rising rate of the output voltage. The regulator goes through the start-up sequence as well after the $\overline{\mathrm{SHDN}}$ pin is pulled to HI .

## Frequency Selection

The EL7516 switching frequency can be user selected to operate at either at constant 620 kHz or 1.25 MHz . Connecting $\mathrm{F}_{\text {SEL }}$ pin to ground sets the PWM switching frequency to 620 kHz . When connect $\mathrm{F}_{\text {SEL }}$ high or $\mathrm{V}_{\text {DD }}$, switching frequency is set to 1.25 MHz .

## Shut-Down Control

When shut-down in is pulled low, the EL7516 is shut-down reducing the supply current to $<3 \mu \mathrm{~A}$.

## Maximum Output Current

The MOSFET current limit is nominally 1.5 A and guaranteed 1.3A. This restricts the maximum output current IOMAX based on the following formula:
$\mathrm{I}_{\mathrm{L}}=\mathrm{I}_{\mathrm{L}-\mathrm{AVG}+\left(1 / 2 \times \Delta \mathrm{I}_{\mathrm{L}}\right)}$
where:
$\mathrm{I}_{\mathrm{L}}=$ MOSFET current limit
$\mathrm{L}_{\mathrm{L}-\mathrm{AVG}}=$ average inductor current
$\Delta \mathrm{I}_{\mathrm{L}}=$ inductor ripple current
$\Delta \mathrm{I}_{\mathrm{L}}=\frac{\mathrm{V}_{\text {IN }} \times\left[\left(\mathrm{V}_{\mathrm{O}}+\mathrm{V}_{\text {DIODE }}\right)-\mathrm{V}_{\text {IN }}\right]}{\mathrm{L} \times\left(\mathrm{V}_{\mathrm{O}}+\mathrm{V}_{\text {DIODE }}\right) \times \mathrm{F}_{\mathrm{S}}}$
$\mathrm{V}_{\text {DIODE }}=$ Schottky diode forward voltage, typically, 0.6 V
$\mathrm{F}_{\mathrm{S}}=$ switching frequency, 600 KHz or 1.2 MHz
$I_{L-A V G}=\frac{I_{O U T}}{1-D}$
$\mathrm{D}=$ MOSFET turn-on ratio:

$$
\mathrm{D}=1-\frac{\mathrm{V}_{\mathrm{IN}}}{\mathrm{~V}_{\mathrm{OUT}}+\mathrm{V}_{\mathrm{DIODE}}}
$$

The following table gives typical maximum lout values for 1.2 MHz switching frequency and $22 \mu \mathrm{H}$ inductor:

TABLE 1.

| $\mathbf{V}_{\mathbf{I N}}(\mathbf{V})$ | $\mathbf{V}_{\text {OUT }}(\mathbf{V})$ | $\mathbf{I}_{\text {OMAX }}(\mathrm{mA})$ |
| :---: | :---: | :---: |
| 2.5 | 5 | 570 |
| 2.5 | 9 | 325 |
| 2.5 | 12 | 250 |
| 3.3 | 5 | 750 |
| 3.3 | 9 | 435 |
| 3.3 | 12 | 330 |
| 5 | 12 | 650 |
| 5 |  | 490 |

## Thermal Performance

The EL7516 uses a fused-lead package, which has a reduced $\theta_{\mathrm{JA}}$ of $100^{\circ} \mathrm{C} / \mathrm{W}$ on a four-layer board and $115^{\circ} \mathrm{C} / \mathrm{W}$ on a two-layer board. Maximizing copper around the ground pins will improve the thermal performance.

This device also has internal thermal shut-down set at around $130^{\circ} \mathrm{C}$ to protect the component.

## Layout Considerations

To achieve highest efficiency, best regulation and most stable operation, a good printed circuit board layout is essential. It is strongly recommended that the demoboard layout to be followed as closely as possible. Use the following general guidelines when laying out the print circuit board:

1. Place $\mathrm{C}_{4}$ as close to the $\mathrm{V}_{\mathrm{DD}}$ pin as possible. $\mathrm{C}_{4}$ is the supply bypass capacitor of the device.
2. Keep the $\mathrm{C}_{1}$ ground, GND pin and $\mathrm{C}_{2}$ ground as close as possible.
3. Keep the two high current paths a) from $\mathrm{C}_{1}$ through $\mathrm{L}_{1}$, to the $L X$ pin and GND and $b$ ) from $C_{1}$ through $L_{1}, D_{1}$, and $\mathrm{C}_{2}$ as short as possible.
4. High current traces should be short and as wide as possible.
5. Place feedback resistor close to the FB pin to avoid noise pickup.
6. Place the compensation network close to the COMP pin.

The demo board is a good example of layout based on these principles; it is available upon request.

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